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#### (57) Abstract

Extrusion coating structure in which at least one layer is made of a polymer composition comprising a multimodal ethylene polymer, which contains from 80 to 100 % by weight of ethylene repeating units and from 0 to 20 % by weight of  $C_3$ – $C_{10}$  alpha–olefin repeating units, has a density of between 0.920 and 0.960 kg/m<sup>3</sup>, and which is a blend of at least two different ethylene polymers.

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### Extrusion coating structure

The invention relates to a multimodal ethylene polymer based extrusion coating composition and its use for coating a paper or board substrate.

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The purpose of this invention is to provide a polyethylene composition for extrusion coating having good processability and good mechanical properties.

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The normal polyethylene extrusion coating grades currently in the market, are low density polyethylenes obtained from high pressure process. Typically, such low density polyethylenes have good processability, but inferior environmental stress crack resistance (ESCR) and seal strength as well as poor hot tack when compared with linear polyethylenes.

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Also some linear polyethylenes, high density, medium density and linear low density polyethylenes are used in extrusion coating applications. However, the extrusion coating compositions are normally prepared by blending linear materials with high pressure low density polyethylene in order to achieve sufficient processability. The problem with linear materials is their poor processability. That has been overcome to some extent by blending the linear material with high pressure low density polyethylene. The benefit of linear polyethylenes is their better mechanical strength allowing thinner coatings.

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The addition of high pressure low density polyethyllene (PE-LD) to linear high density or low density polyethylene (PE-HD or PE-LLD) usually leads to a loss in mechanical and barrier properties. Another drawback of blends is the extra cost caused due to the additional compounding step, where the blend of PE-HD or PE-LLD and high pressure PE-LD is made.

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The idea of the present invention is to use a bimodal or multimodal linear polyethylene material in extrusion coating without adding any high pressure PE-LD. The bimodality

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or multimodality of the ethylene polymer of this invention ensures a sufficient throughput while the superior mechanical properties of linear polyethylenes are maintained. The material is especially suitable for coextrusion.

The purpose of the invention has been achieved with a polymer composition comprising 5 a multimodal ethylene polymer, which contains from 80 to 100 % by weight of ethylene repeating units and from 0 to 20 % by weight of C<sub>3</sub>-C<sub>10</sub> alpha-olefin repeating units, has a density of between 0.920 and 0.960 g/cm3, and which is a blend of at least two different ethylene polymers.

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By a multimodal ethylene polymer is in connection with the present invention meant an ethylene polymer having broad molecular weight distribution produced by blending two or more ethylene polymer components with different molecular weights or by polymerizing ethylene to different molecular weights in a process with two or more reactors in series. By contrast, a unimodal polyethylene, like those conventionally used in extrusion coating, is obtained from only one ethylene polymer component produced in only one step.

The extrusion coating composition according to the present invention is a multimodal ethylene polymer. The multimodal ethylene polymer is by definition a blend of at least two ethylene polymers having different molecular weights. According to an important embodiment of the present invention, said blend is the product of polymerization process comprising at least two steps. In the process, the first ethylene polymer is prepared by polymerizing ethylene in the presence of a catalyst system in the first step and the second polymer is prepared by (co)polymerizing ethylene and optionally a 25 higher alpha olefin in the presence of a catalyst system in the second step. Said steps can be performed in any order.

The idea of the present invention can be realized with any kind of ethylene polymerization catalyst, such as chromium catalyst, a Ziegler-Natta catalyst or a

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metallocene catalyst. Typical catalyst systems are e.g prepared according to WO91/12182 and WO95/35323 which are herewith included by reference. A preferential single site polymerization catalyst system is that based on a group 4 metal metallocene and alumoxane.

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When performing said polymerization process comprising at least two steps, one or more catalyst systems, which may be the same or different, can be used. It is preferential, if the blend of ethylene polymers is the product of the polymerization process, that the same catalyst system is used in the subsequent steps.

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The most convenient way to control the molecular weight during the multistep polymerization is to use hydrogen, which acts as a chain-transfer agent by intervening in the insertion step of the polymerization mechanism. Hydrogen may be added in suitable amounts to any step of the multistep polymerization.

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It is prior known to prepare multimodal and especially bimodal olefin polymers in two or more polymerization reactors in serie. Such processes are exemplified by EP 040992, EP041796, EP 022376 and WO92/12182 which are hereby included as reference concerning the preparation of multimodal ethylene polymers for the claimed extrusion coating material. According to these references each of said polymerization step can be performed in liquid phase, slurry or gas phase.

According to the present invention, it is preferential to perform said polymerization steps as a combination of slurry polymrization and gas phase polymerization. Preferentially the first step is a slurry polymerization and the second step a gas phase polymerization.

The slurry polymerization is preferentially performed in a so called loop reactor. The gas phase polymerization is performed in a gas phase reactor. The polymerization steps can optionally be preceded by a prepolymerization, whereby up to 20 % by weight and

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preferentially 1-10 % by weight of the total ethylene polymer amount is formed.

According to another important embodyment of the invention, the multimodal ethylene polymer can be produced by mixing at least two ethylene polymers having different average molecular weights.

A suitable melt flow rate MFR<sub>2</sub> of the ethylene polymer blend is between 1 and 30 g/10 min.

The molecular weight distribution curve of a multimodal ethylene polymer shows either several peaks or a broad peak lacking small fractions of extremely low and extremely high molecular weight fractions.

Of course, the finished polymerization or mixing product can be further treated to modify its average molecular weight and molecular weight distribution according to the application to which the material is used.

The polymer composition of this invention is suitable for extrusion coating of fiber based materials like paper and paperboard. The grammage of paper or paperboard substrate is typically  $20 \text{ g/m}^2$  -  $400 \text{ g/m}^2$ .

The substrate used in the extrusion coating can also be a plastic film made of polyester, polyamide, cellophane, polypropylene and oriented polypropylene. When using plastic film substrate, the thickness is typically 10  $\mu m$  - 80  $\mu m$ .

In addition, also aluminium subtrate can be used and then the thickness of substrate is from 6  $\mu m$  to 300  $\mu m.$ 

The polymer composition according to this invention can be used as the only extrusion coating layer over the substrate or it can be used in multilayer products as one layer or

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several layers.

Depending on the final product, it is, of course, possible to use extrusion coating structures in which the multimodal ethylene polymer blend is used together with certain other polyethylene. That other ethylene polymer can be a high pressure low density ethylne polymer or copolymer or a unimodal linear ethylene polymer. The multimodal polymer and the other polymer are mixed before the extrusion coating.

The invention is described in more detail in the following examples.

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Materials used in the examples:

LE7518 = PE-LD coating grade, MFR<sub>2</sub>= 7.5 g/10 min, density  $0.918 \text{ g/cm}^3$ .

LE4524 = PE-LD coating grade,  $MFR_2 = 4.5 \text{ g}/10 \text{ min}$ , density 0.923 g/cm<sup>3</sup>

Dowlex3010 = PE-LLD, manufacturer Dow

Polymer A = Medium density multimodal ethylene polymer

Polymer B = Linear low density multimodal ethylene polymer

Polymer C = Linear low density multimodal ethylene polymer

Properties of polymers A, B and C are given in Table 1.

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All polymers except Dowles3010 are manufactured by Borealis Polymers Oy.

Table 1

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Polymer	A	В	С
Loop MFR, g/10 min	130	100	100
Loop density, kg/m <sup>3</sup>	960	941	941
Final MFR, g/10 min	10	13	9
Final density, kg/cm <sup>3</sup>	942	930	931
FRR21/2	41	37	39

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Production of multimodal polymers:

#### Example 1 (Polymer A):

In a loop reactor was produced polyethene with MFR<sub>2</sub> 130 g/10 min and density 960 kg/m<sup>3</sup>. Then, the polymer containing the active catalyst was transferred into a gas phase reactor where the polymerization was continued in such conditions that the MFR<sub>2</sub> of the final polymer A was 10 g/10 min, density 942 kg/m<sup>3</sup> and FRR21/2 was 41.

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## Example 2 (Polymer B):

In a loop reactor was produced polyethene with  $MFR_2$  100 g/10 min and density 941 kg/m<sup>3</sup>. Then, the polymer containing the active catalyst was transferred into a gas phase reactor where the polymerization was continued in such conditions that the  $MFR_2$  of the final polymer B was 13 g/10 min, density 930 kg/m<sup>3</sup> and FRR21/2 was 37.

#### Example 3 (Polymer C):

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In a loop reactor was produced polyethylene with MFR<sub>2</sub> 100 g/10 min and density 941  $kg/m^3$ . Then, the polymer containing the active catalyst was transferred into a gas phase reactor where the polymerization was continued in such conditions that the MFR<sub>2</sub> of the final polymer C was 9 g/10 min, density 931  $kg/m^3$  and FRR21/2 was 39.

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#### Coating tests:

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#### Example 4

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Coating test runs were carried out using a Beloit -pilot extrusion coating line. In test runs two extruders with L/D 24D/114 mm screws, max. output 450 kg/h of each, were used.

All tested samples were first processed to monolayer coatings, meaning that same material was used in both extruders. The same method was applied to testing of dry blends of higher density multimodal polymers (=polymer A) and basic PE-LD coating grade. The proportion of PE-LD in dry blends was 15 w-%.

During the coating process of multimodal MD product (polymer A) it was seen that the motorload of extruders was lower compared to processing of present extrusion coating PE-LLD grade (Dowlex3010). The maximum screw speed with Polymer A was 100 rpm, while with normal PE-LLD grade only level of 90 rpm was reached. The benefit becomes stronger when the melt temperature setting for the multimodal medium density ethylene polymer (A) was lower (300 °C) than the same setting for normal PE-LLD (315 °C).

The multimodal products of lower density level (=polymer B and C) were tested besides monolayer testing also as coextrusion materials. In coextrusion testing extruder I was used for PE-LD and extruder II for multimodal material. In that way multimodal material became the outer layer of the structure. All tests were made with both polymers B and C.

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The optimal melt temperature setting was searched regarding to MFR<sub>2</sub> of each tested sample. The materials were tested with various coating weights and line speeds. The substrate used in all tests was brown 70 g/m<sup>3</sup> UG-paper.

Coating weight variation, edge weaving of the coating polymer and neck-in values were

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all in very reasonable level with LE7518 +multimodal LLD (B and C) coextruded structures. It was seen during the test runs that support layer of 2 g/m<sup>2</sup> LE7518 with multimodal LLD (polymer B and C) layer being 8 g/m<sup>2</sup> is adequate.

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There were plenty of advantages compared to high pressure PE-LD extrusion coating polymers, when examinating the final-product properties of multimodal materials. Especially, the hot tack strength was clearly in a higher level; the value of coextruded LE7518+multimodal LLD (B and C), 15 + 15 g/m² structure, was 3.5 N/15 mm when PE-LD LE4524 has a value 2.5 N/15 mm. The puncture strength index for coextruded multimodal LLD was 4.9, while LE4524 has the index 3.1. The elongation in machine direction for multimodal LLD coextruded was 6.3 % compared to only 2.1 % for LE4524. Also the cross direction elongation was clearly better, value was 9.2 %, while LE4524 has a limit in 4.7 %. There are no pinholes in coextruded multimodal LLD coatings even when the coating weight was as low as 10 g/m² (2g/m²LE7518+8g/m² polymer C).

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#### Claims:

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- 1. Extrusion coating structure **characterized in that** at least one layer is made of a polymer composition comprising a multimodal ethylene polymer, which contains from 80 to 100 % by weight of ethylene repeating units and from 0 to 20 % by weight of C<sub>3</sub>-C<sub>10</sub> alpha-olefin repeating units, has a density of between 0.920 and 0.960 g/cm<sup>3</sup>, and which is a blend of at least two different ethylene polymers.
- 2. Extrusion coating structure according to claim 1 **characterized in that** the ethylene polymer blend is a product of a process in which the first ethylene polymer is prepared by polymerizing ethylene in the presence of a catalyst system in the first step and the second polymer is prepared by polymerizing ethylene in the presence of a catalyst system in the second step.
- 3. Extrusion coating structure according to claim 1 **characterized in that** the ethylene polymer blend is produced by mixing at least two ethylene polymers having different average molecular weights.
- 4. Extrusion coating structure according to claims 1-3 **characterized in that** the melt flow rate MFR<sub>2</sub> of the ethylene polymer blend is between 1 and 30 g/10 min.
  - 5 Extrusion coating structure according to claims 1-4 **characterized in that** the substrate of the coating structure is fiber based like paper or paperboard.
- 6. Extrusion coating structure according to claim 5 **characterized in that** the grammage of paper or paperboard substrate is 20 g/m<sup>2</sup> 400 g/m<sup>2</sup>.
  - 7. Extrusion coating structure according to claims 1-4 **characterized in that** the substrate of the coating is a plastic film made of e.g. polyester, polyamide, polypropylene or cellophane.

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- 8. Extrusion coating structure according to claim 7 characterized in that the thickness of the plastic film substrate is  $10 \mu m 80 \mu m$ .
- 9. Extrusion coating structure according to claims 1-4 **characterized in that** the substrate of the coating is made from aluminium.
  - 10. Extrusion coating structure according to claim 9 characterized in that the thickness of the aluminium substrate is from 6  $\mu$ m to 300  $\mu$ m.
- 11. Extrusion coating structure according to any of the preceding claims **characterized**in that the ethylene polymer blend is used as the only coating layer in an extrusion coating structure.
- 12. Extrusion coating structure according to any of the preceding claims **characterized**in that the ethylene polymer blend is used as layer in a coextruded coating structure.
  - 13. Extrusion coating structure according to claim 12 **characterized in that** the layer made from the ethylene polymer blend is used as nearest to the substrate, as a mediate layer or as a surface layer.
  - 14. Extrusion coating structure according to any of the preceding claims **characterized** in that the ethylene polymer blend is used mixed with certain other polyethylene.
- 15. Extrusion coating structure according to claim 14 **characterized in that** the other ethylene polymer is high pressure low density ethylne polymer or copolymer.
  - 16. Extrusion coating structure according to claim 14 **characterized in that** the other ethylene polymer is unimodal linear ethylene polymer.

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## A. CLASSIFICATION OF SUBJECT MATTER IPC6: C08L 23/08, B32B 27/32 According to International Patent Classification (IPC) or to both national classification and IPC B. FIELDS SEARCHED Minimum documentation searched (classification system followed by classification symbols) IPC6: CO8L Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched SE,DK,FI,NO classes as above Electronic data base consulted during the international search (name of data base and, where practicable, search terms used) WPI C. DOCUMENTS CONSIDERED TO BE RELEVANT Relevant to claim No. Citation of document, with indication, where appropriate, of the relevant passages Category\* 1 - 16WO 9703124 A1 (BOREALIS POLYMERS OY), P,X30 January 1997 (30.01.97), abstract 1-16 US 5674342 A (TODD J. OBIJESKI ET AL), P,X 7 October 1997 (07.10.97), claims US 5338589 A (LUDWIG BÖHM ET AL), 16 August 1994 (16.08.94), column 1, line 62 - column 2, line 2, 1 - 16X column 3, line 48 - line 60, claims 1 and 13 Further documents are listed in the continuation of Box C. See patent family annex. Х later document published after the international filing date or priority Special categories of cited documents: date and not in conflict with the application but cited to understand the principle or theory underlying the invention "A" document defining the general state of the art which is not considered to be of particular relevance "X" document of particular relevance: the claimed invention cannot be "E" erlier document but published on or after the international filing date considered novel or cannot be considered to involve an inventive step when the document is taken alone document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "Y" document of particular relevance: the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination "O" document referring to an oral disclosure, use, exhibition or other being obvious to a person skilled in the art document published prior to the international filing date but later than "&" document member of the same patent family the priority date claimed Date of mailing of the international search report Date of the actual completion of the international search **29** -04-1998 20 April 1998 Authorized officer Name and mailing address of the ISA/ Swedish Patent Office Box 5055, S-102 42 STOCKHOLM Monika Bohlin

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